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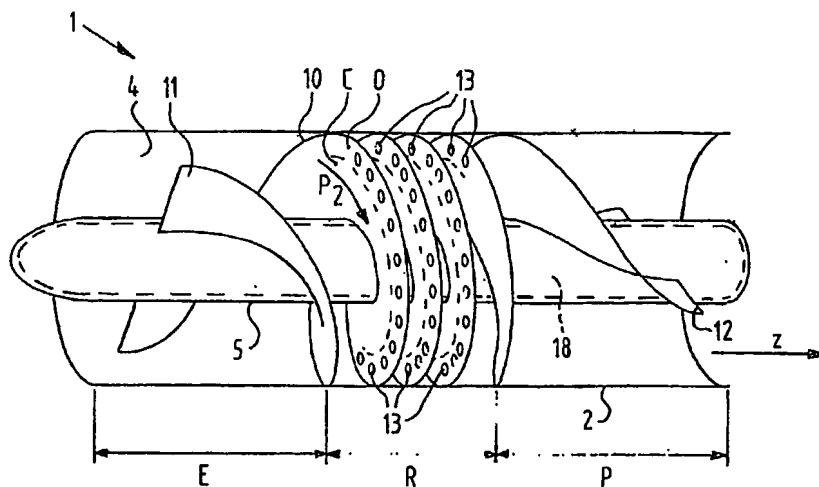
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(54) Title: SEPARATOR FOR SEPARATING A SOLID, LIQUID AND/OR GAS MIXTURE



(57) Abstract: The invention relates to a cyclone separator for separating a mixture containing solid particles, liquid and/or gas into a heavy fraction and a light fraction, the separator comprising: - a casing (2) defining a flow space through which the mixture is to flow; - an elongated flow body (5) arranged in the flow space along which the mixture to be separated can be carried; - at least one swirl inducing element (10) arranged between the flow body and the inner casing, the swirl inducing element being curved so as to set the incoming mixture into a rotating movement for the purpose of separating the mixture into the heavy fraction and the light fraction; - discharge means for discharging the separated heavy and light fraction, wherein the discharge means comprise at least one flow passage defined inside said at least one swirl element.

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SEPARATOR FOR SEPARATING A SOLID, LIQUID AND/OR GAS MIXTURE

5 The present invention relates to a cyclone separator for separating a mixture containing solid particles, liquid and/or gas into a heavy fraction and a light fraction.

 Separating devices for separating such mixtures, such as mixtures of oil and gas, are known in which use is made of
10 the differences in specific weight of the parts of which the mixture is made up. A cyclone separator generally consists of a tube in which a central flow body is arranged. Provided on the flow body are guide fins with which the mixture flowing into the tube under overpressure is brought into rotation. As
15 a result of the centrifugal forces occurring due to the rotation, the relatively heavy fraction of the mixture is flung outward, while the relatively light fraction of the mixture is displaced in a zone along the flow body. Because the light and heavy fractions are displaced in separate
20 zones, a separation of the mixture can be effected by arranging outlet provisions at a suitable location, and the separated light and heavy fractions can be discharged separately.

 Cyclone separators are used in a large number of
25 situations. Inlet cyclones are for instance applied in gravity separation vessels. Inlet cyclones ensure that the incoming mixture undergoes a determined pretreatment before a further separation takes place. The inlet cyclones is connected for this purpose to the inlet of the gravity
30 separation vessel and is provided with an outlet for the heavy fraction and an outlet for the light fraction, wherein both outlets debouch in the interior of the gravity separation vessel for further separation of the mixture. An

example of an inlet cyclone is described in the European patent application EP 1 187 667 A2.

Another type of cyclone separator is the so-called in-line separator in which the incoming mixture and at least a part of the outgoing mixture flows through a pipeline, wherein the separator is essentially aligned with the pipeline. In-line cyclone separators can be subdivided into two different types.

In a first type, also known as a "degasser", the separator separates gas from liquid. The degasser is used, in the case of the gas/liquid mixture, when the continuous phase is liquid. An example of a degasser is known from WO 01/00296 A1. In the degasser the liquid continuous flow is set into rotation by a number of guide blades causing swirling. Because of the difference in density between the gas and liquid and the initiated centrifugal field, the gas is urged to the middle of the separator, this producing a stable core of gas. Removal of the gas core is brought about by means of a gas discharge pipe arranged in the middle of the cyclone and provided with outlet openings. Because of the geometry of the separator removal of the gas via the outlet openings takes place in radial direction.

A second type of in-line cyclone separator is a separator, also referred to as a "deliquidiser", in which a gas continuous feed is set into rotation by a number of guide blades causing swirling. The deliquidiser in this case separates the liquid from the gas. The liquid is urged in the direction of the pipe wall, which results in a stable liquid film (layer) which is displaced in the direction of the gas outlet. In the outlet zone the gas and the liquid are separated at a fixed position in the flow. The gas outlet is a cylindrical open pipe which is fixed in the flow space of the separator. The gas is discharged in longitudinal

direction. An example of a deliquidiser is described in WO 02/056999 A1.

A drawback of the known cyclone separators is that they are relatively bulky, since provisions must be made in the separator for separate discharge of the separated heavy fraction and the separated light fraction. These provisions are usually made downstream of the guide fins, which entails a relatively large minimum length of such cyclone separators.

It is an object of the present invention to provide an improved cyclone separator in which the above stated drawback is obviated.

Provided for this purpose according to the invention is a cyclone separator for separating a mixture containing solid particles, liquid and/or gas into a heavy fraction and a light fraction, wherein the separator comprises:

- a casing defining a flow space through which the mixture is to flow, the casing having an inlet for the mixture to be separated and an outlet for the discharge of either the heavy or light fraction of the mixture;
- an elongated flow body arranged in the flow space along which the mixture to be separated can be carried;
- at least one swirl-inducing element arranged between the flow body and the inner casing, the swirl-inducing element being curved so as to set the incoming mixture into a rotating movement for the purpose of separating the mixture into the heavy fraction and the light fraction;
- discharge means for discharging the separated heavy and light fraction, wherein the discharge means comprise at least one flow passage defined inside said at least one swirl element.

By making use of the space inside the swirl element, such as for instance a guide fin which is wholly or partially hollow or in which one or more channels are provided, at

least one of the two fractions (i.e. either the light or the heavy fraction) can already be discharged at the position of the swirl elements, this enhancing the compactness of the cyclone separator.

5 In the above-mentioned cyclone separator known in the professional field as a degasser, the light fraction is guided inward downstream of the guide fins into a discharge tube extending centrally in longitudinal direction of the cyclone tube, and is subsequently guided in the direction of
10 the downstream outer end of the cyclone tube. The heavy fraction also continues on its way in longitudinal direction. Although this degasser produces a good separating result, the degasser is quite large in longitudinal direction. In order to reduce the dimensions of such a degasser there is provided
15 according to a further aspect of the invention a cyclone separator, comprising:

- at least one second flow passage defined inside the flow body and connecting to the first flow passage in the swirl element;

20 - an outer casing arranged around the inner casing, the outer and inner casing defining a third flow passage connected to the first flow passage;

wherein the discharge means further comprise one or more openings in the flow body, the openings connecting to the
25 second flow passage inside the flow body so as to discharge the separated light fraction through the openings and the second, first and third passage respectively.

In this cyclone separator the light fraction is therefore discharged via the flow body, the swirl element and a second
30 flow space arranged around the first flow space. This means that a separator can be realized which is very compact in longitudinal direction, which makes the cyclone separator particularly suitable for well-head applications. Because

optimal use can moreover be made of the available space, a lower pressure drop occurs over the cyclone separator.

According to a further preferred embodiment, the openings are provided in a region close to the downstream end of the flow body. Close to the downstream end of the flow body the mixture has covered a great distance (or separation length) such that the mixture is well separated.

According to a further preferred embodiment, the flow body has a converging portion at the downstream end thereof, so that a gradual discharge of the light fraction can be realized. This form of the flow body moreover prevents a suction effect from the outlet, which could have an adverse effect on the separation result.

In a particular embodiment the openings in the flow body are provided only in the converging portion of the flow body. No openings are arranged in the other, substantially cylindrical portion of the flow body. Only separation takes place at the position of the cylindrical portion, while discharge takes place at the position of the converging portion. This embodiment is particularly favourable when relatively little gas (less than about 20%) is present in the liquid, in the case of a solid/liquid separator such as a sand/liquid separator.

In another embodiment in which the flow body has a substantially cylindrical portion and a converging portion the openings are provided in both the cylindrical portion and converging portion. A first separation therefore already takes place at the position of the cylindrical portion. This embodiment is particularly favourable when a relatively large amount of gas (up to 80% or more) is present in the liquid in the case of a solid/liquid separator such as a sand/liquid separator. It has been found that the separating efficiency

increases considerably when openings are arranged not only in the converging portion but also in the cylindrical portion.

According to a further preferred embodiment, the converging portion of the flow body has a substantially conical shape. Said inner casing preferably also has a converging form. This produces a heavy fraction outlet with a small cross-section so that the least possible light fraction (for instance liquid in a sand/liquid separator) is entrained with the heavy fraction (sand in said sand/liquid separator) and is discharged via the heavy fraction outlet.

According to a further preferred embodiment, the mutual distance between the inner casing and the flow body is substantially constant. This has a stabilizing effect on the flow. When the speed downstream of the swirl elements threatens to decrease as a result of friction, the separator can be embodied so that the mutual distance in flow direction (longitudinal direction) even decreases slightly, which brings about an increase in speed so as to compensate the decrease in speed resulting from friction.

The non-prepublished application NL 1 028 238 of applicant describes a cyclone separator in which the heavy fraction is discharged via openings arranged in the cyclone tube, while the light fraction continues on its way through the cyclone tube and can be discharged via the outer end thereof. This document also describes a cyclone separator in which the light fraction is discharged by providing discharge openings in the flow body which communicate with a channel extending through the flow body and a discharge pipe connected thereto. The light fraction is discharged via openings in this passage, while the heavy fraction continues on its way through the cyclone tube and can be discharged at the outer end of the cyclone tube.

In both embodiments of the known cyclone separator the heavy fraction or light fraction must be discharged respectively via the wall of the cyclone tube or via the flow body. The part of the heavy fraction that is relatively far removed from the inner surface of the cyclone tube and the part of the light fraction that is relatively far removed from the outer surface of the flow body can however be less readily "captured" by the discharge openings, which in some situations has an adverse effect on the separation efficiency of the cyclone.

It is also an object of the present invention to obviate this drawback.

According to a further aspect of the invention there is provided for this purpose a cyclone separator in which the discharge means further comprise:

- one or more openings in the swirl element, the openings connecting to the first flow passage;
- a second flow passage connected to the first flow passage in said at least one swirl element, the second flow passage extending to an outlet for discharge of the heavy or light fraction, the other fraction to be discharged from the outlet of the casing.

An improved discharge of the heavy fraction or the light fraction can be achieved by placing the discharge openings in the swirl element itself. A greater or smaller part of the light or heavy fraction can moreover be discharged as desired by a correct dimensioning and/or positioning of the discharge openings in the swirl element.

It is noted that said openings in the swirl element can be provided instead of the above-mentioned openings in the cyclone tube and/or the flow body. In other embodiments the discharge openings are provided in the cyclone tube, the swirl element and/or the flow body.

According to a first preferred embodiment, the openings are provided in a circumferential zone adjacent the cyclone tube so as to guide the heavy fraction through the first and second flow passages to the outlet of the second flow passage. When the openings are arranged in this zone, the heavy fraction is therefore discharged via the swirl element. In another preferred embodiment the openings are provided in a circumferential zone adjacent the flow body so as to guide the light fraction through the first and second passages to the outlet of the second flow passage. In this embodiment the light fraction is therefore discharged via the swirl element.

According to a further preferred embodiment, the second flow passage is defined inside the flow body, for instance by making the flow body wholly or partially hollow or by providing one or more channels therein. The relevant fraction (heavy or light fraction) can hereby be discharged in a structurally simple manner and without adversely affecting the flow in the flow space around the flow body.

Irrespective of where the openings are arranged in the swirl element, the second flow passage can also be defined between the inner casing and a second outer casing arranged around the inner casing. In this embodiment the fraction (light or heavy fraction) discharged via the openings is not discharged inward via the flow body but is discharged radially outward via a second flow space present around the above-mentioned flow space. In this embodiment a very compact construction method can be realized, i.e. the length of the cyclone separator can be relatively short.

Further advantages, features and details of the present invention will be elucidated on the basis of the following description of the preferred embodiments thereof. Reference is made in the description to the accompanying figures, in which:

figure 1 shows a partially cut-away view in perspective of a first preferred embodiment of the cyclone separator according to the present invention;

figure 2 is a longitudinal section of the first preferred embodiment shown in figure 1 of the cyclone separator according to the present invention;

figure 3 is a partially cut-away view in perspective of a second preferred embodiment of the cyclone separator according to the present invention;

10 figure 4 is a partially cut-away view in perspective of a third preferred embodiment of the cyclone separator according to the present invention;

figure 5 is a longitudinal section of the third preferred embodiment shown in figure 4 of the cyclone separator according to the present invention;

figure 6 shows a partially cut-away view in perspective of a fourth preferred embodiment of the cyclone separator according to the present invention;

figure 7 is a longitudinal section of the fourth preferred embodiment of the cyclone separator shown in figure 6;

figure 8 shows a partially cut-away line drawing in perspective of a fifth preferred embodiment of the cyclone separator according to the present invention;

25 figure 9 is a partially cut-away view in perspective of the fifth preferred embodiment of figure 8; and

figure 10 is a partially cut-away line drawing of a sixth preferred embodiment of the cyclone separator according to the invention.

30 The embodiments of the separators according to the invention as shown in figures 1-6 are particularly, though not exclusively, intended for separating a gas phase (gas phase vapour) from a liquid phase (water/oil), for instance

in a pipeline leading to an oil platform. As indicated above, the separators can however be used to separate the random mixtures of one or more liquids, one or more gases and/or one or more different types of solid particle. Figures 8-10 for instance show separators which are particularly, though not exclusively, suitable for sand/liquid separation (wherein gas may also be present to greater or lesser extent in the liquid).

Figures 1 and 2 show a first embodiment of a separator 1 comprising a cyclone tube 2 which is provided at its proximal end with an inlet 3 for connecting to the feed part of a pipeline (not shown). Provided at the distal end of cyclone tube 2 is an outlet 3' for connecting to a discharge part of the pipeline (not shown). Arranged in the flow space 4 defined in the interior of tube 2 is a central flow body 5 which extends in axial direction (z-direction as shown in figure 1). A curved guide fin 10 is arranged between the inner surface of tube 2 and the outer surface of flow body 5.

Three different regions are defined between the proximal end 11 and distal end 12 of guide fin 10. An entry region (E) is defined extending in downstream direction from the proximal end. A pressure recovery region (P) is defined extending in downstream direction from the rear end 12 of guide fin 10, while an intermediate region or removal region 25 is defined in the region between entry region (E) and pressure recovery region (P). The function of the guide fin in entry region (E) is to set into rotation (as shown by arrow P_2 in figure 1) the incoming mixture (figure 2, P_1) flowing along guide fin 10.

30 In order to bring about the rotating movement of the mixture the angle α , which is defined as the angle between the axial direction (z-direction) and guide fin 10 on the outer surface of flow body 5, begins with a value of about 0

degrees, and this angle increases gradually in order to increase the curvature of the guide fin. In the intermediate region @ said angle α remains constant, or almost constant, in order to allow the mixture to rotate at a more or less equal rotation speed. In the pressure recovery region (P) the angle α is gradually reduced from the value in the intermediate region to substantially 0 degrees in order to reduce the rotation of the mixture flowing along guide fin 10.

10 In the shown embodiment an edge of each guide fin is fixed to the inner surface of the tube or casing 2, while the opposite edge of guide fin 10 is fixed to flow body 5. Other setups are however also possible, for instance wherein the guide fins are only fixed to flow body 5.

15 In the shown embodiments the mixture rotates clockwise. It will be understood that in other embodiments (not shown) rotation can also take place in counter-clockwise direction.

As a result of the curvature of guide fin 10 in entry region (E) a part of the mixture, i.e. the relatively heavy fraction of the mixture, is flung outward by the rotating movement and this part is transported to a substantially annular outer zone O (figure 2) once it has reached the intermediate region R. Another part of the mixture, i.e. the relatively lightweight part thereof, will remain in a central zone or core zone C. In figures 1 and 2 the boundary between the outer zone O and zone C is indicated with a broken line. In practice however, there is no abrupt boundary between the two zones. There is in fact a transition region between the two zones.

30 The relatively heavy fraction of the mixture which is present in the entry region in the flow space and which is flung outward eventually comes to lie in the intermediate region @ at one or more openings or perforations 13 provided

in guide fin 10. The heavy fraction is discharged (P_3) via these openings 13 to a hollow space 15 inside guide fin 10 and discharged via this hollow space 15 to the inner flow passage 8 provided in flow body 5. In the shown embodiment
5 the flow passage is formed by embodying flow body 5 at least partially as a hollow tube. In other embodiments (not shown) the passages through flow body 5 are embodied in one or more channels or tubes arranged in or on flow body 5.

The inner flow passage 11 can be connected to a discharge
10 pipe 14 via which in this case the heavy fraction can be discharged (P_4 - P_6). In the shown embodiment the light fraction of the incoming mixture remains in the inner zone C and does not therefore come onto that part of guide fin 10 where openings 13 are situated. The light fraction continues on its
15 way (P_7) and is discharged via outlet 3' (P_8).

Figure 3 shows a second preferred embodiment of the invention wherein openings 16 in guide fin 10 are provided in inner zone C. Because openings 13 are provided in this embodiment in the inner zone, the openings will function as
20 discharge for the light fraction present in this zone C. In similar manner as described above for the first embodiment, the light fraction that has come to lie in central region C is discharged via the passage 15 provided in guide fin 10 and passage 11 provided in the flow body in the direction of
25 discharge pipe 14, via which the light fraction can be discharged.

Figures 4 and 5 show a third preferred embodiment of the invention in which passage(s) 16 inside guide fin 10 is (are) in flow connection with a second flow space 17 outside
30 cyclone tube 2. In this preferred embodiment the separated fraction which has entered via the openings, instead of being carried radially inward in the direction of flow body 5, is carried outward in radial direction to the second flow space

17. When discharge openings 13 are for instance provided in the outer zone (O), and the openings therefore discharge the heavy fraction, the heavy fraction is discharged radially outward in the direction of the second flow space 17 (P_{10}) and then discharged in longitudinal direction of the separator (P_{11}). The light fraction situated in the central area C continues on its way along the first flow space and is discharged at the outer end thereof (P_{12}).

When conversely the discharge openings 13 are provided in the inner central region C, these openings functioned as discharge for the light fraction. This embodiment is shown for instance in figures 6 and 7. In this embodiment the light fraction, having entered the inner space of guide fin 10, is discharged radially outward (P_{10}) in the direction of the second flow space 17 and subsequently discharged in longitudinal direction of the second flow space (P_{11}). In the first to the fourth embodiments of the invention referred to herein the calculated separation results, in view of the fact that the cyclone provides a stable flow, are very similar to the measured separation values, which enables a good optimization of the cyclone for a specific application.

The fifth, particularly advantageous preferred embodiment of the invention shown in figures 8 and 9 likewise has this advantage. This preferred embodiment is particularly suitable for separating a sand/liquid mixture, wherein the light phase (the liquid) is discharged via an inner pipe and the guide fin(s). Cyclone separator 20 consists of an elongate inner tube 21 (shown partially cut-away) and an outer tube 22 arranged concentrically therearound. A flow space 23 is defined between the outer surface of inner tube 21 and the inner surface of outer tube 22. A substantially annular dividing wall 24 is provided at the upstream outer end of the outer and inner tube 22, 21, so that flow space 23 is closed

at that end. The dividing wall 24 can be fixed to a flange 25, this flange being provided with fastening openings 26 with which the flange can be fixed to the outer end of a pipe (not shown) of a pipeline. Likewise arranged on the opposite 5 outer end of separator 20 is a flange 27 provided in similar manner with fastening openings 28 for fixing a following pipe (not shown) of the pipeline. A flow body 30 is arranged in inner tube 21. In the shown embodiment this flow body 30 is an elongate tube which has at its upstream outer end a 10 converging, in the shown embodiment conically shaped part 40. For the sake of clarity in the drawing a part of the tube of flow body 30 is shown cut-away. In reality however, flow body 30 is closed (except of course for the openings which provide access to the guide fins and openings 41 on the outer end of 15 the flow body, as will be set forth later).

Guide fins 31 and 32 are arranged in the outer surface of flow body 30 and/or on the inner surface of inner tube 21. Each of the guide fins 31, 32 comprises an upstream part 33 extending practically in axial direction of separator 20 and 20 a curved downstream part which ensures that the mixture flowing therealong is set into rotation. In the interior of each of the guide fins 31, 32, preferably (though not limited thereto) in the upstream part 35 thereof, there are provided channels 36 which are connected on one side to inner space 35 25 of flow body 30 and which are connected on the other side via openings 37 to flow space 23 between inner tube 21 and outer tube 22.

Openings are arranged at the position of the converging portion 40 of the flow body. In the shown embodiment the 30 openings are curved slots 41, these openings providing access from flow space 29, which is defined between the outer surface of flow body 30 and the inner surface of inner tube 21, to the interior 35 of flow body 30.

Close to converging portion 40 of flow body 30, and in the shown embodiment slightly downstream thereof, inner tube 21 is likewise provided with converging portion 45 so that the intermediate distance between the outer surface of flow body 30 and the inner surface of inner tube 21 remains almost constant, also in the region where the converging portion 40 of flow body 30 is situated. The flow space 29 debouches into a discharge pipe 46 which is arranged and extends almost centrally in the flow space and which in turn runs out into a discharge pipe 47 along which a part of the mixture can be discharged, as will be set forth below. Flow space 23 between the outer surface of inner tube 21 and the inner surface of outer tube 22 debouches into a relatively wide part 23' at the distal end 46 of separator 20 in order to discharge the part of the mixture flowing therein in the direction of the following part of the pipeline (not shown).

In use the mixture for separating enters at the proximal end 47 of separator 20 (P_{13}) and passes into flow space 29. The mixture under pressure continues on its way and flows along the outer side of flow body 30 until the mixture reaches guide fins 31, 32. Guide fins 31, 32 set the mixture flowing therealong into rotation (P_{14}), whereby in known manner the mixture makes a rotating movement in flow space 29. The relatively heavy parts, for instance the solid particles in a sand/liquid separator, come to lie in a region close to the inner surface of inner wall 21, while the relatively light parts of the mixture, i.e. in the present embodiment the liquid, comes to lie in a region close to the outer surface of the flow body. When the light fraction reaches the conical outer end 40 of flow body 30 provided with openings 41, the light fraction is discharged radially (P_{15}) and then axially (P_{16}) in the direction of the proximal part 47 of the separator. The light fraction is thus sent

back in the direction of channels 36 provided in the guide fins. As stated above, there is a free passage between inner space 35 of flow body 30 and the flow space 23 between outer tube 22 and inner tube 21. As a consequence the light

5 fraction is carried via channels 36 to flow space 23 (P_{17}) and subsequently discharged via flow space 23' (direction P_{18}) in the direction of the distal end 46 of the separator. There the separated light fraction is discharged (P_{19}) via the pipeline (not shown).

10 The heavy fraction on the other hand, which as a result of the centrifugal forces makes a rotating movement close to the inner surface of inner tube 21, remains in flow space 29 and enters (P_{19} , P_{20} and P_{21}) the above-mentioned discharge tube 46. This discharge tube 46 discharges the heavy fraction
15 via outlet 47 (P_{22}). In this manner a very compact separator can be realized which is fully aligned with the pipeline (a so-called in-line separator).

Figure 10 shows a sixth preferred embodiment of the cyclone separator. This embodiment is almost wholly similar
20 to the fifth embodiment of the separator described above, so that a detailed description of the operation of the separator - to the extent it is the same as that of the fifth embodiment - can be dispensed with here. In the present
25 embodiment not only are openings 41 arranged in the distal part 40 of the flow body, but openings 50 are also provided in the more proximally located cylindrical portion 49 of the flow body. Particularly when the light phase (liquid/gas in a solid/liquid separator) contains a relatively large amount of gas, the additional openings 50 in the flow body produce an
30 improved discharge of the light fraction, which enhances the separation efficiency to be achieved by the cyclone separator.

The present invention is not limited to the preferred embodiments thereof described herein. The right sought are rather defined by the following claims, within the scope of which many modifications can be envisaged.

CLAIMS

1. Cyclone separator for separating a mixture containing solid particles, liquid and/or gas into a heavy fraction and
5 a light fraction, the separator comprising:

- a casing defining a flow space through which the mixture is to flow, the casing having an inlet for the mixture to be separated and an outlet for the discharge of either the heavy or light fraction of the mixture;
- 10 - an elongated flow body arranged in the flow space along which the mixture to be separated can be carried;
- at least one swirl-inducing element arranged between the flow body and the inner casing, the swirl-inducing element being curved so as to set the incoming mixture into a
15 rotating movement for the purpose of separating the mixture into the heavy fraction and the light fraction;
- discharge means for discharging the separated heavy and light fraction, wherein the discharge means comprise at least one flow passage defined inside said at least one swirl
20 element.

2. Cyclone separator as claimed in claim 1, comprising:

- at least one second flow passage defined inside the flow body and connecting to the first flow passage in the swirl element;
 - 25 - an outer casing arranged around the inner casing, the outer and inner casing defining a third flow passage connected to the first flow passage;
- wherein the discharge means further comprise one or more openings in the flow body, the openings connecting to the
30 second flow passage inside the flow body so as to discharge the separated light fraction through the openings and the second, first and third passage respectively.

3. Cyclone separator as claimed in claim 2, wherein the openings are provided in a region close to the downstream end of the flow body.

4. Cyclone separator as claimed in claim 2 or 3, wherein
5 the flow body has a converging portion at the downstream end thereof.

5. Cyclone separator as claimed in any of the claims 2-4, wherein the converging portion has a substantially conical shape.

10 6. Cyclone separator according to claim 4 or 5, wherein the openings are provided in the converging portion only.

7. Cyclone separator according to claim 1, wherein the flow body includes a substantially cylindrical portion and a converging portion, the openings being provided in both the
15 cylindrical portion and converging portion.

8. Cyclone separator as claimed in any of the claims 2-6, wherein the inner casing has a converging portion.

9. Cyclone separator as claimed in any of the claims 2-6, wherein the mutual distance between the inner casing and the
20 flow body is substantially constant along the separator.

10. Cyclone separator as claimed in claim 1, wherein the discharge means further comprise:

- one or more openings in the swirl element, the openings connecting to the first flow passage;

25 - a second flow passage connected to the first flow passage in said at least one swirl element, the second flow passage extending to a second flow passage outlet for discharge of the heavy or light fraction, the other fraction to be discharged from the outlet of the casing.

30 11. Cyclone separator as claimed in claim 10, wherein the openings are provided in a circumferential zone adjacent the casing so as to guide the heavy fraction through the first

and second flow passages to the outlet of the second flow passage.

12. Cyclone separator as claimed in claim 10 or 11, wherein the openings are provided in a circumferential zone adjacent the flow body so as to guide the light fraction through the first and second passages to the outlet of the second flow passage.

13. Cyclone separator as claimed in any of the claims 10-12, wherein the second flow passage is defined inside the flow body.

14. Cyclone separator as claimed in any of the claims 10-13, wherein the second flow passage is defined between the inner casing and a second outer casing arranged around the inner casing.

15. Cyclone separator as claimed in any of the preceding claims, wherein the inner and outer casings are substantially tubular and the passage between the inner and outer casing is substantially annular.

16. Cyclone separator as claimed in any of the claims 2-15, wherein the one or more openings are elongated openings extending substantially parallel to the local main flow direction of the mixture.

17. Cyclone separator as claimed in any of the preceding claims, wherein the separator is adapted to be arranged between pipes of a pipeline so as to constitute a part of a pipeline.

18. Cyclone separator as claimed in claim 1, wherein the separator can be mounted so as to be aligned with the pipeline.

19. Gravity separation vessel provided with at least one cyclone separator as claimed in any of the preceding claims.

20. Method of separating a mixture containing solid particles, liquid and/or gas into a heavy fraction and a light fraction, the method comprising the steps of:

a) providing a cyclone separator comprising:

- 5 - a casing defining a flow space through which the mixture is to flow, the casing having an inlet for introducing the mixture to be separated and an outlet for discharging the heavy fraction of the mixture;
- an elongated flow body arranged in the flow space
- 10 along which the mixture to be separated can be carried;
- at least one swirl-inducing element arranged between the flow body and the inner casing, the swirl-inducing element being curved so as to set the incoming mixture into a rotating movement for the purpose of
- 15 separating the mixture into the heavy fraction and the light fraction;
- discharge means for discharge of the light fraction, the discharge means comprising at least one flow passage defined inside said at least one swirl element, at
- 20 least one second flow passage defined inside the flow body and connecting to the first flow passage in the swirl element, at least one third flow passage connected to the first flow passage, the third flow passage being defined between an outer casing arranged around the inner casing, and
- 25 one or more openings in the flow body, the openings connecting to the second flow passage inside the flow body;
- b) guiding the mixture to be separated through the said inlet;
- c) setting the mixture into a rotating movement, causing
- 30 the mixture to be separated into a heavy fraction and a light fraction;
- d) guiding the separated light fraction through the openings in the flow body;

e) guiding the light fraction backwards through the second passage inside the flow body;

f) guiding the light fraction from the second passage through the first passage in the swirl element;

5 g) discharging the light fraction through the third passage between the outer and inner casing;

h) discharging the heavy fraction through said outlet of the inner casing.

21. Method according to claim 20, wherein the cyclone
10 separator is a separator according to any of the claims 1-19.

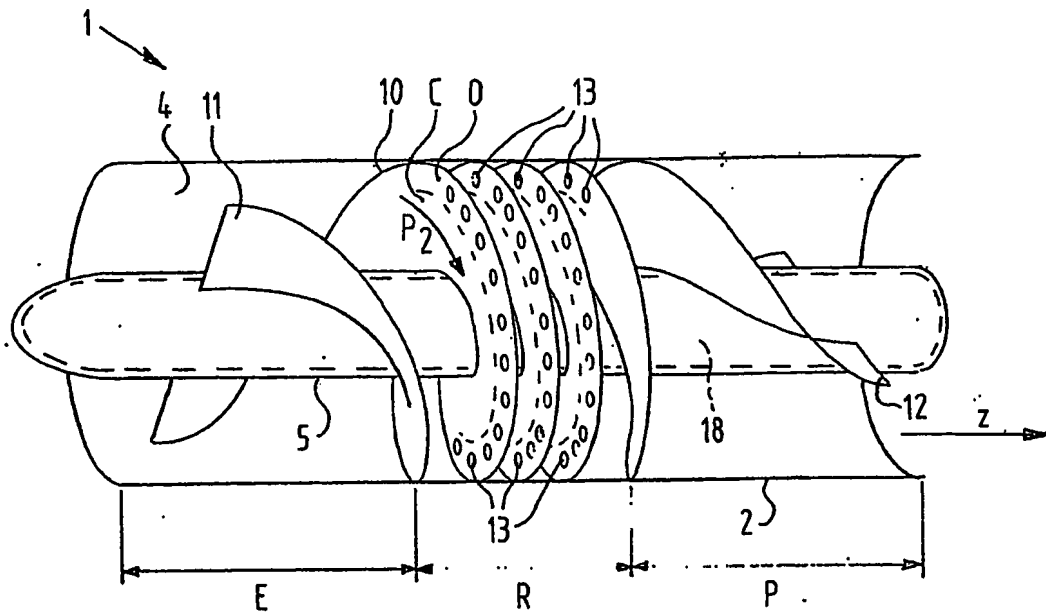


FIG. 1

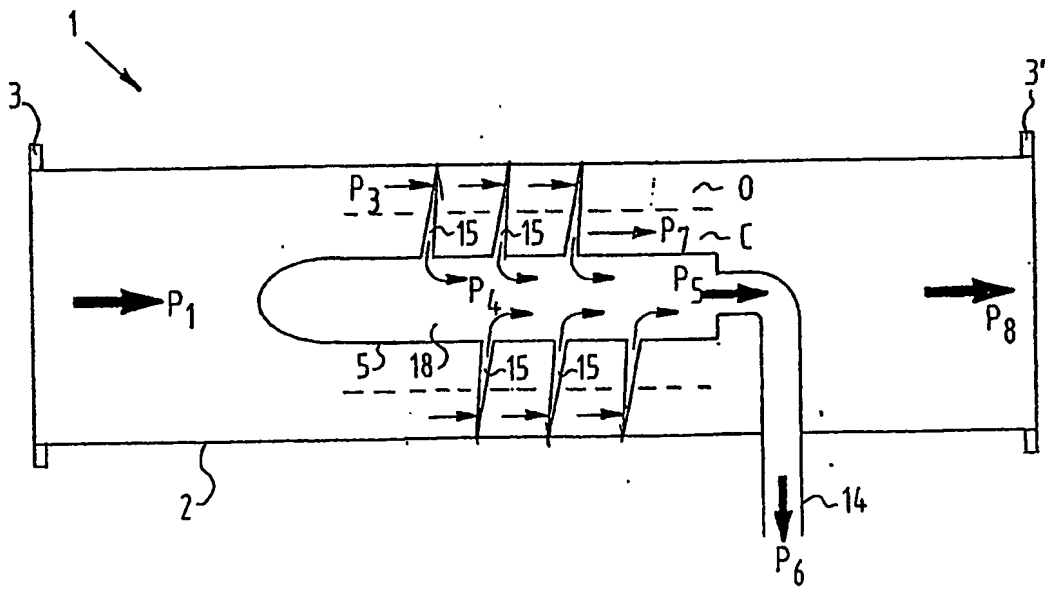


FIG. 2

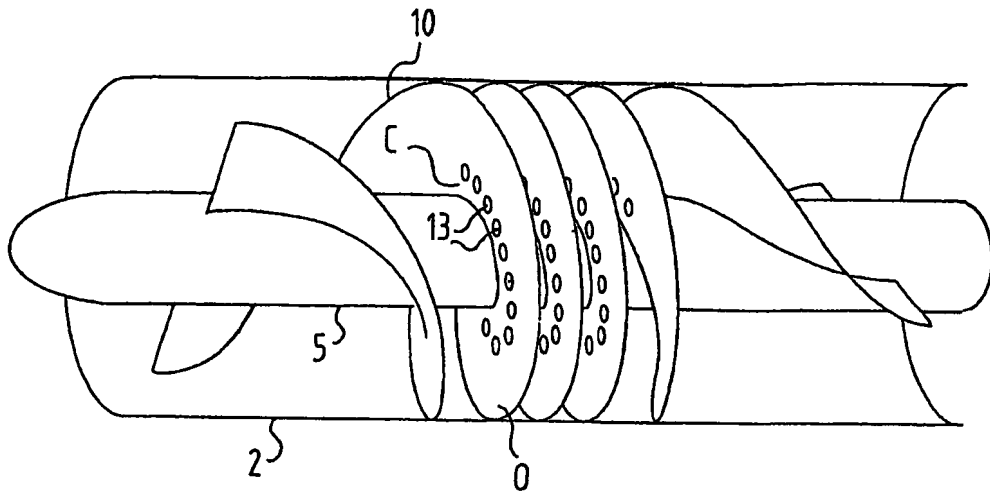


FIG. 3

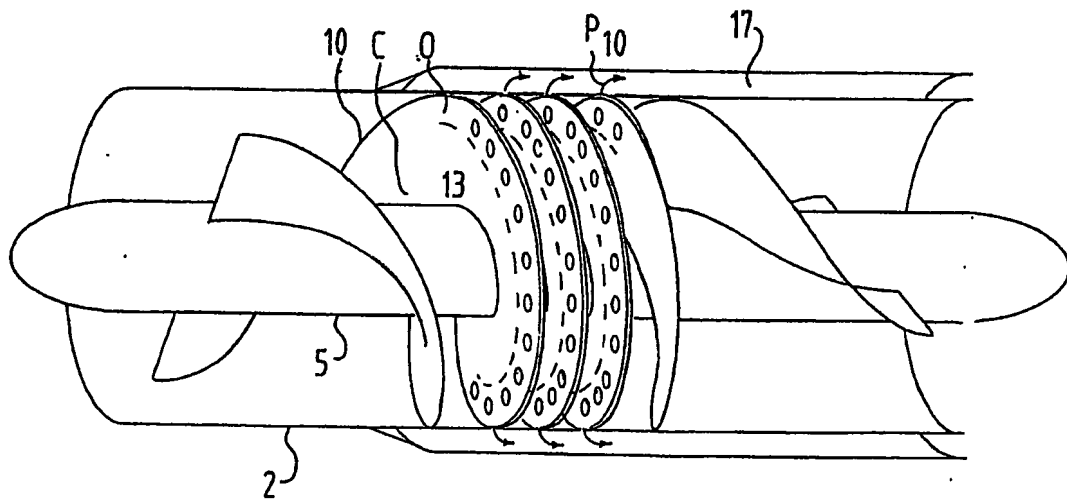


FIG. 4

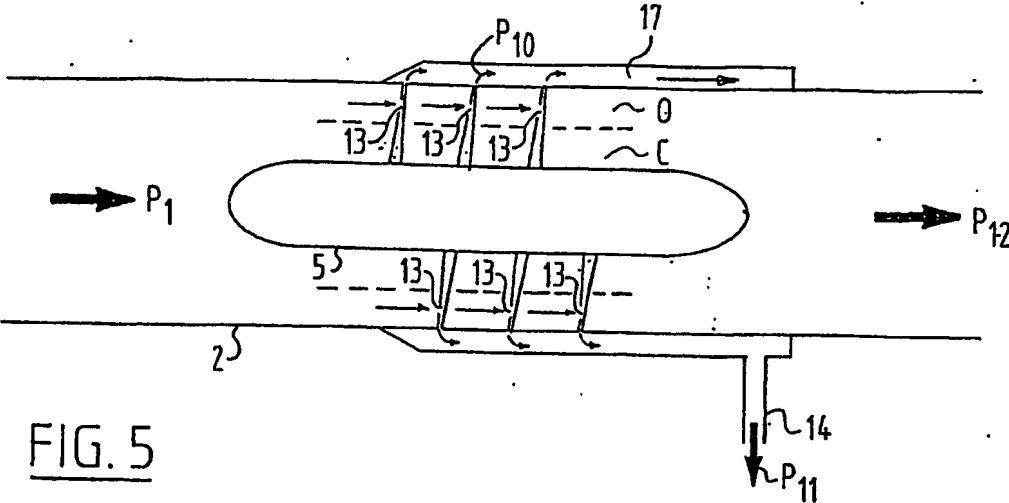


FIG. 5

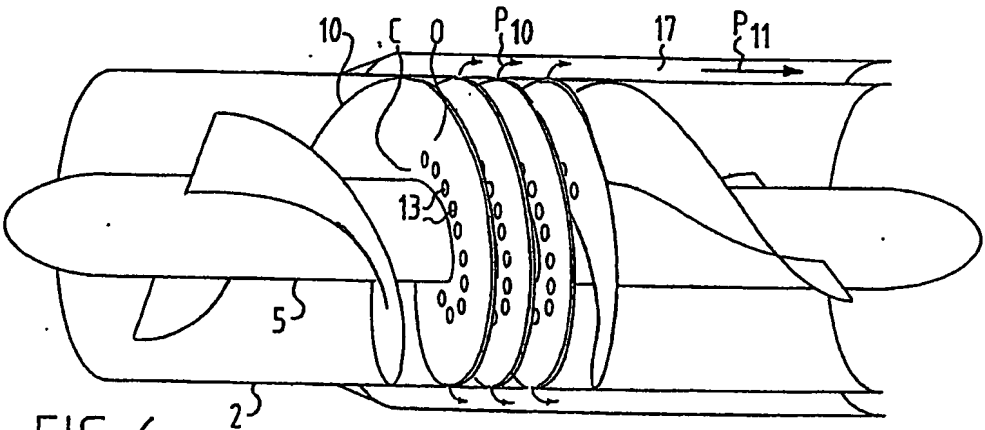


FIG. 6

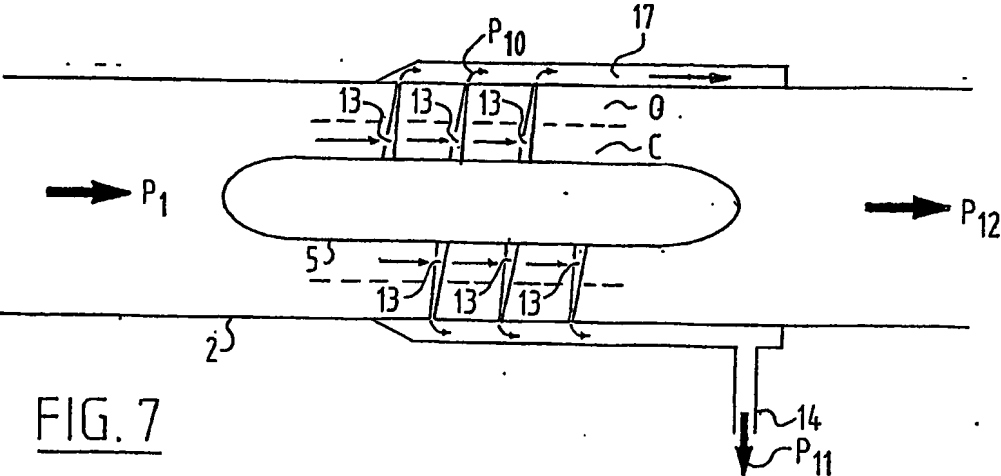


FIG. 7

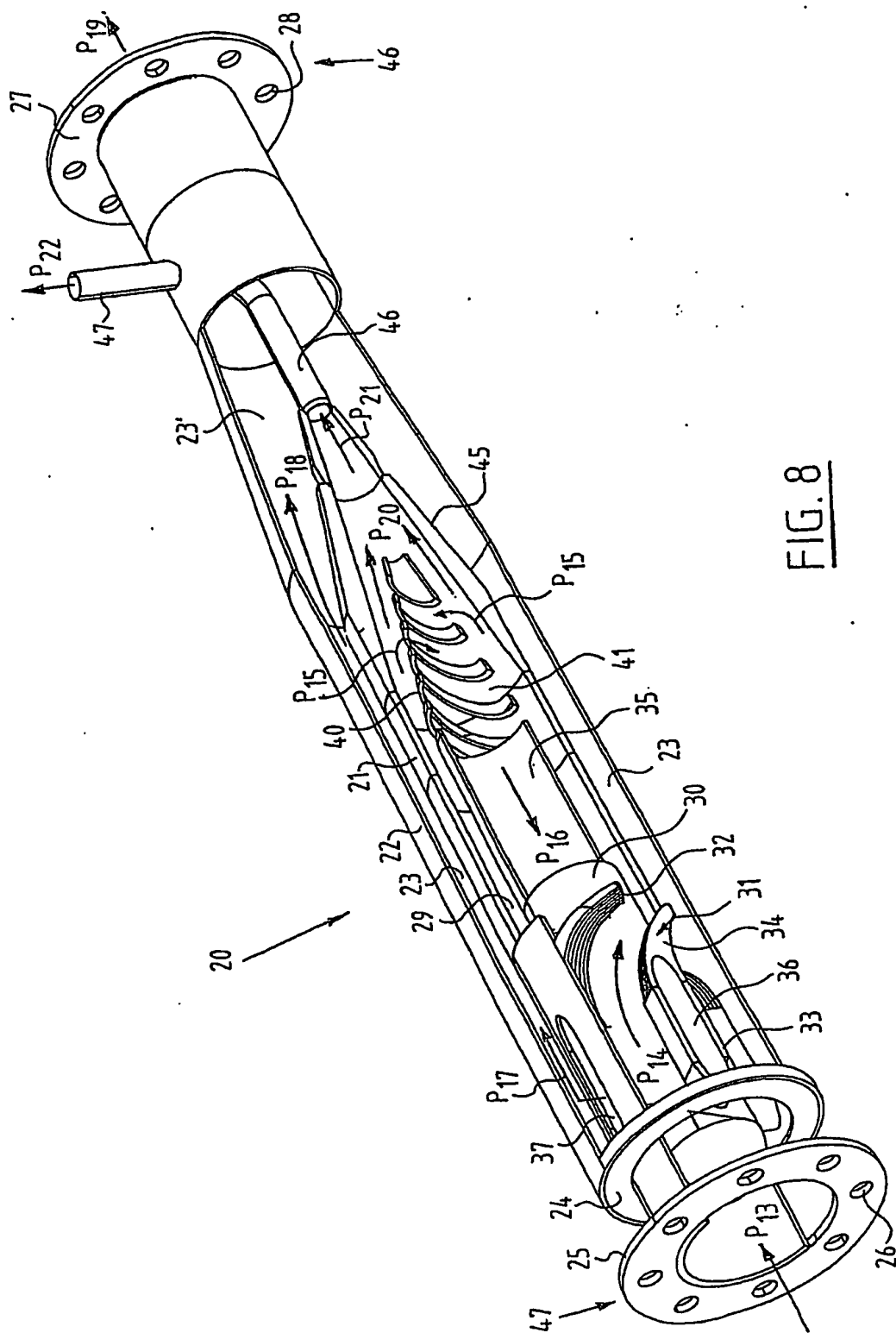


FIG. 8

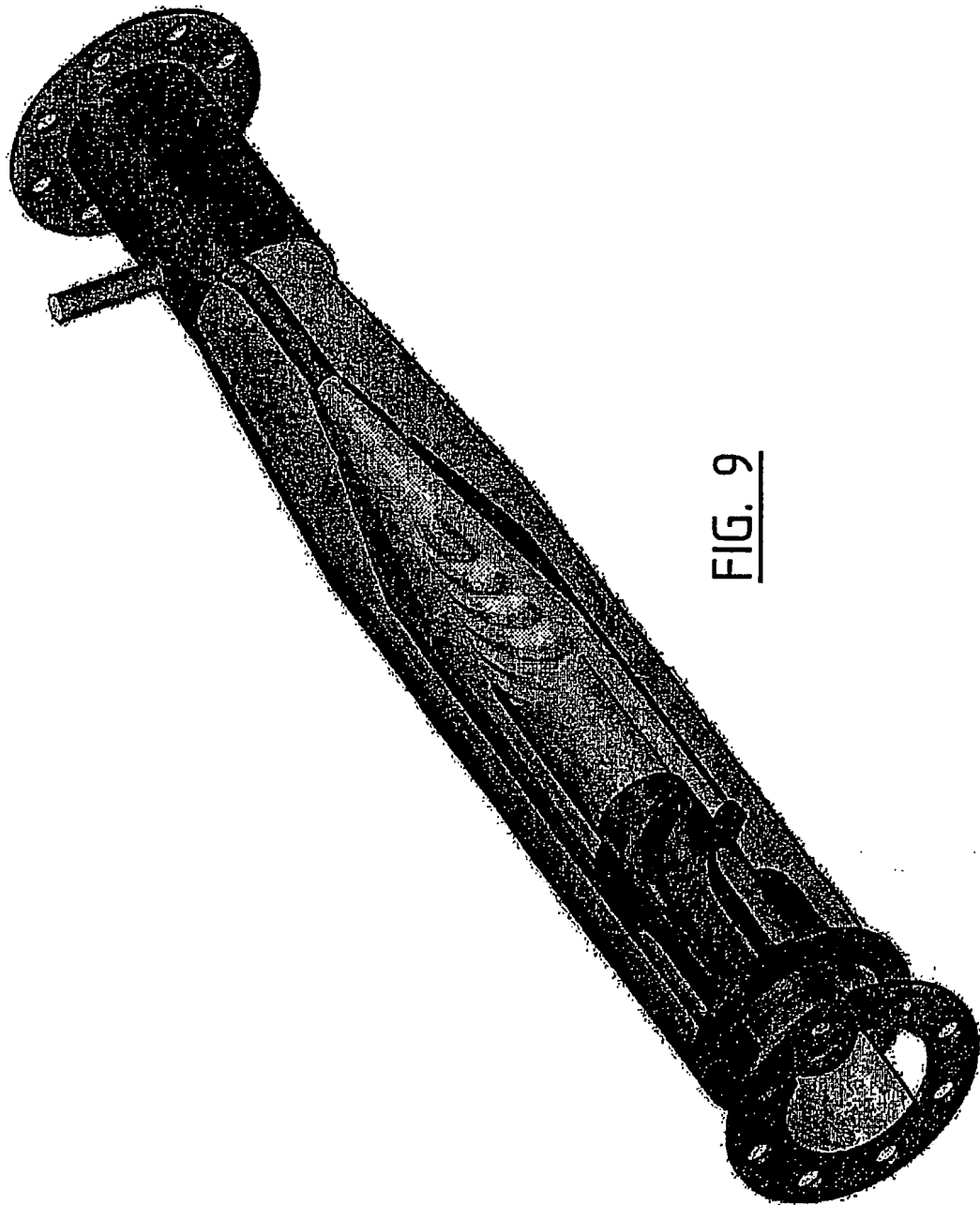


FIG. 9

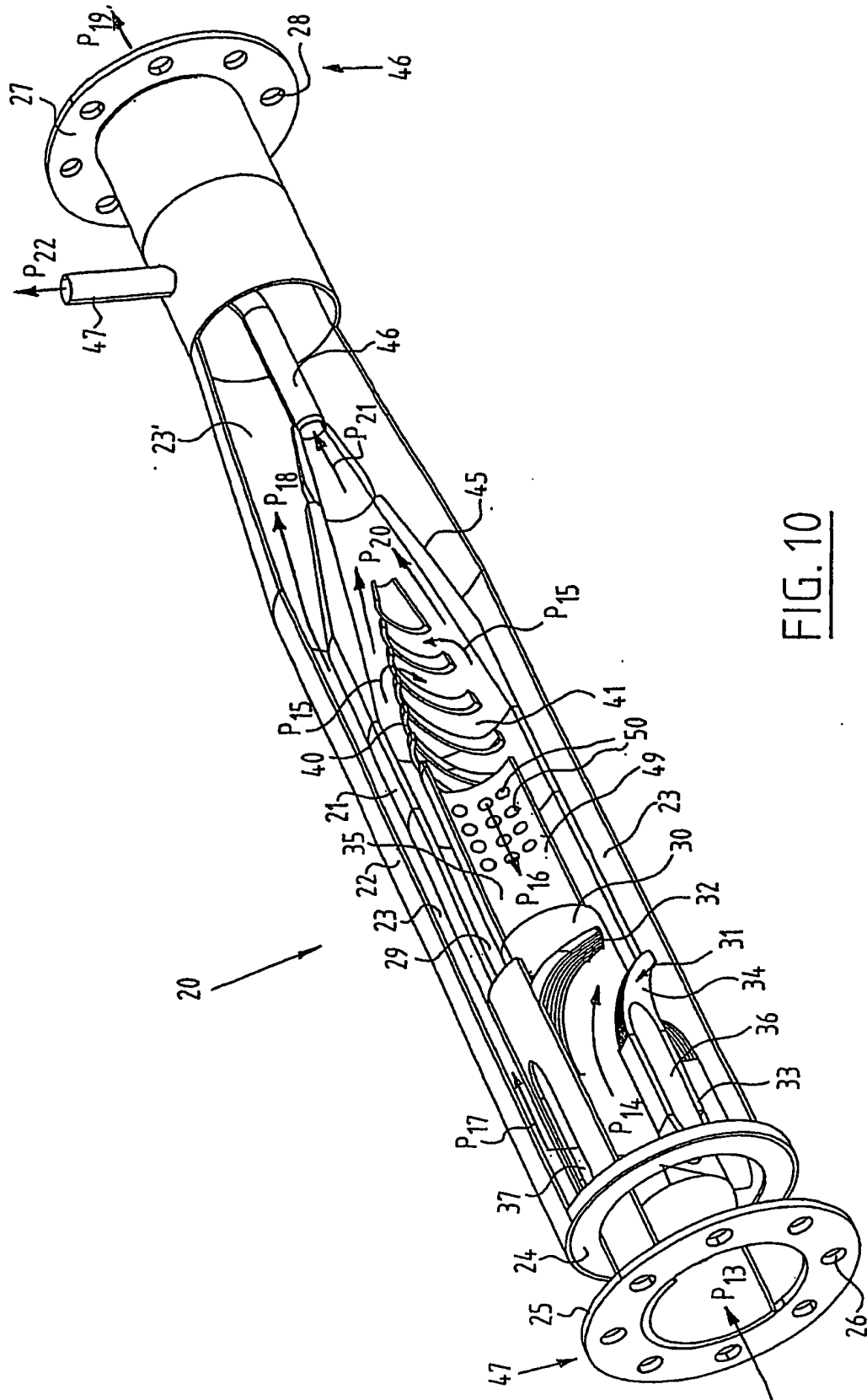


FIG. 10

INTERNATIONAL SEARCH REPORT

International application No
PCT/NL2006/000320

A. CLASSIFICATION OF SUBJECT MATTER

INV. B01D19/00 B01D45/16 B04C3/06 B01D21/26 B01D17/02
E21B43/34

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
B04C B01D E21B

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

EPO-Internal

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	WO 99/43439 A (READ PROCESS ENGINEERING A/S; MICHELET, JAN, FREDRIK) 2 September 1999 (1999-09-02) page 3, line 34 - page 6, line 18; figures -----	1-21
X	US 4 666 476 A (REEVE ET AL) 19 May 1987 (1987-05-19) the whole document -----	1,10, 17-19 20
A	US 3 693 329 A (ROBIN BURKE WILLIS) 26 September 1972 (1972-09-26) the whole document -----	1,17,18 20
A	US 2 847 087 A (JOHNSON JOHN CUNNINGHAM) 12 August 1958 (1958-08-12) -----	
A	US 4 179 273 A (MONTUSI, ROBERT R) 18 December 1979 (1979-12-18) -----	
	----- -/-	

☒ Further documents are listed in the continuation of Box C.

☒ See patent family annex.

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G document member of the same patent family

Date of the actual completion of the international search

11 September 2006

Date of mailing of the international search report

25/09/2006

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INTERNATIONAL SEARCH REPORT

International application No
PCT/NL2006/000320

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT

Category*	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
A	US 2 413 324 A (HOLZWARTH HANS THEODOR) 31 December 1946 (1946-12-31) -----	

INTERNATIONAL SEARCH REPORT

Information on patent family members

International application No

PCT/NL2006/000320

Patent document cited in search report		Publication date	Patent family member(s)	Publication date
WO 9943439	A	02-09-1999	AU 2552799 A EP 1073526 A1 NO 980767 A	15-09-1999 07-02-2001 25-08-1999
US 4666476	A	19-05-1987	EP 0147215 A2 EP 0167583 A1 GB 2151505 A WO 8502782 A1 JP 61501683 T NO 853288 A	03-07-1985 15-01-1986 24-07-1985 04-07-1985 14-08-1986 20-08-1985
US 3693329	A	26-09-1972	NONE	
US 2847087	A	12-08-1958	FR 1154054 A GB 772763 A	02-04-1958 17-04-1957
US 4179273	A	18-12-1979	NONE	
US 2413324	A	31-12-1946	NONE	